





4707700140

WELL NO. 112540  
 SAND BALTIMORE - A.C., Penna.

1000' R.A.  
 95' TEMP  
 160 ACRES

LOG INTERPRETATION

DEPTH	DENSITY		R <sub>t</sub>	NEUTRON				CORE			LOG			PERFORATING DEPTH	
	C/SEC	BULK		INDEX	Ø†	Sw	So	So	Sw	Ø	Ø	Sw	Sg		So
2175	541		70					5	100			7	58		2175 2180
2180	542		70									7	58		86
2980	540		60					5	80			7	42		80 2980
2985			60									7	42		90
2299	570		65					6	80			8	31		96 2300
2305	570		65												
2311	542		45									7	48		2310
15	540		45					4	80			7	48		20

160  
 570  
 570  
 570

WELL NO. 11254

4707700140

SAND ELK 7

LOG INTERPRETATION

DEPTH	DENSITY		R <sub>t</sub>	NEUTRON				CORE			LOG				PERFORATING DEPTH
	C/SEC	BULK		INDEX	Ø†	Sw	So	So	Sw	Ø	Ø	Sw	Sg	So	
5137		2.53	85								61	40	60	AVOID PART 6.2	
38		2.54	80								60	41	58	AVOID SW 40.5	
45		2.53	80								62	42	58	AVOID SW 59.5	
46		2.52	88								68	38	62	Fp 205A	
47		<del>2.55</del>	80								51	162	238	AVOID GPO RESERVE 140MM	
EIK3															
4956		2.55	90												
57		2.54	100												
58		2.54	100												
Balltown															
3170		2.54	40												
71		2.51	50												
72		2.55	60												
73		2.55	55												
74		2.52	52								70	45	55		
75		2.47	55								81	38	62		
76		2.46	60								88	35	65		
77		2.47	70								80	32	68	Ø = 7.6%	
78		2.47	70								80	32	68	Sw = 37%	
79		2.47	70								80	32	68	Sg = 63	
80		2.48	72								79	35	65	Diameter 1920	
81		2.49	71								75	36	69	Fp 1269	
82		2.51	70								70	40	60		
83		2.51	70								70	40	60	Reserve = 350	
84		2.50	70								72	38	62		
85		2.52	65								70	42	58		
86		2.54	52												
											11.5	1950	755		

47077.00(40)

11254

~~Circle~~

Pr. - 5th Ball  
242M

$$43560 \times \frac{1041}{1053} \times (1 - \frac{89}{100}) \times \frac{.876}{.876} \times 15.325 \times (460 + \frac{116}{95}) \times \frac{160}{160} \text{ Ac.} =$$

$$\begin{array}{r} \times \frac{563160}{7450.7} \times \frac{541300}{7914} \\ \times 75.6 \text{ G8A} \end{array}$$

$$3175-80 \quad \frac{476,720,640}{526,701,560} \times .07 \times \frac{.62}{.55} \times 5^{\circ} = 103450 \quad \underline{114,340}$$

$$2980-2988 \quad \times .07 \times \frac{.55}{.42} \times 8' = 151840 \quad \underline{171136}$$

$$2299-2305 \quad \times .08 \times .66 \times 6' = 151,026 \quad \underline{166,920}$$

$$2311-15 \quad \times .07 \times .52 \times 4' = 69412 \quad \underline{76,716}$$

$$\begin{array}{r} 475,728 \quad 529,112 \\ \textcircled{350} \quad \times 85\% \\ \hline 449,145 \text{ MCF} \end{array}$$

NC

GL =  $.684 \times 2739 = 1873$

Wellhead \* =  $\frac{960}{1020} + 15 = \frac{975}{1015}$

Res. Press.  $\frac{1041}{1053}$

Gv. =  $.684$

Per. =  $.672$

Tcr. =  $.352$

Pr. =  $\frac{1041}{1053} = 1.55$

Tr =  $\frac{672}{546} = 1.67$

Z =  $.876$

4707700140

11254

Pr. - 5th Ball  
o) 242M

$$43560 \times \frac{1041}{1043} \times (1 - \frac{897}{876}) \times 15.325 \times (460 + \frac{116}{95}) \times 160 \text{ Ac.} =$$

$$\times \frac{562160}{7450.7} \times \frac{541320}{79.18}$$

$$\times 75.6 \text{ GGA}$$

$$3125-80 \quad \frac{476,720,640}{526,901,760} \times 0.7 \times 3.6 \times 5 = 103450 \quad 114,340$$

$$2980-2986 \quad \times 0.7 \times 4.8 \times 8' = 151840 \quad 171136$$

$$2299-2305 \quad \times 0.08 \times 6.6 \times 6' = 151,026 \quad 166,920$$

$$2311-15 \quad \times 0.7 \times 5.2 \times 4' = 69412 \quad 76,716$$

$$475,728 \quad 529,112$$

(350) ✓

$$\times 85\%$$

$$449,145 \text{ BCF}$$

NC

$$GL = .684 \times 2739' = 1873$$

$$\text{Wellhead} * = \frac{960}{1000} + 15 = \frac{975}{1015}$$

$$\text{Res. Press.} \quad \frac{1041}{1033}$$

$$Gv. = .684$$

$$Pcr. = 672$$

$$Tcr. = 352$$

$$Pr. = \frac{1041}{1030} = 1.01$$

$$Tr = \frac{672}{576} = 1.17$$

$$Z = .876 \text{ 80\%}$$